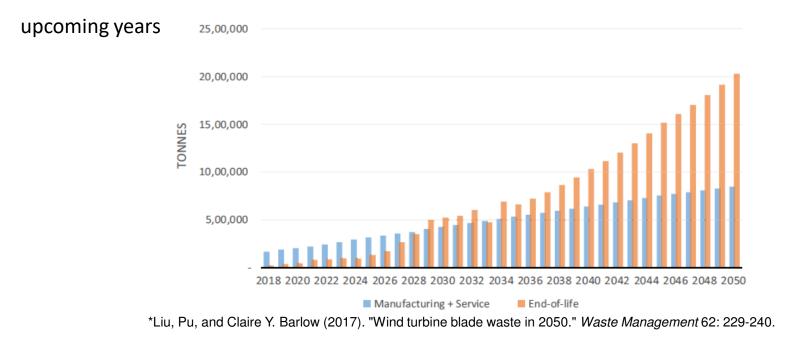


Properties of a 37 m long FRP wind turbine blade after 11 years in service

Alshannaq, A. A., Respert, J. A., Bank, L. C., Gentry, T. R., & Scott, D. W.

Re-wind.info larry.bank@design.gatech.edu

□ Large amounts of wind blade composite materials are expected to be disposed of in the



These are non-biodegradable materials, and are harmful to the environment to dispose of them. Sustainable solutions to deal with wind blade waste are needed.

How do we deal with Wind Blade Waste?

- □ "DISPOSAL" through incineration or landfilling
 - > Environmentally harmful option with no positive societal impact
 - I "RECYCLING" using mechanical, thermal or chemical processing
 - Replacements for virgin constituents in new composites or cementitious mortars and concretes
 - Economical viability and reduced properties are the main drawbacks
- □ A new option explored in this research: "REPURPOSING"
 - Which includes characterizing, developing, analyzing, and prototyping applications where large-scale/full-scale parts of the wind blades are utilized in civil infrastructure

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*Suhail, Raj, Jian-Fei Chen, T. R. Gentry, B. Tasistro-Hart, Y. Xue, and L. C. Bank (2019). "Analysis and design of a pedestrian bridge with decommissioned FRP windblades and concrete." *Fiber Reinforced Polymers in Reinforced Concrete Structures FRPRCS14*.

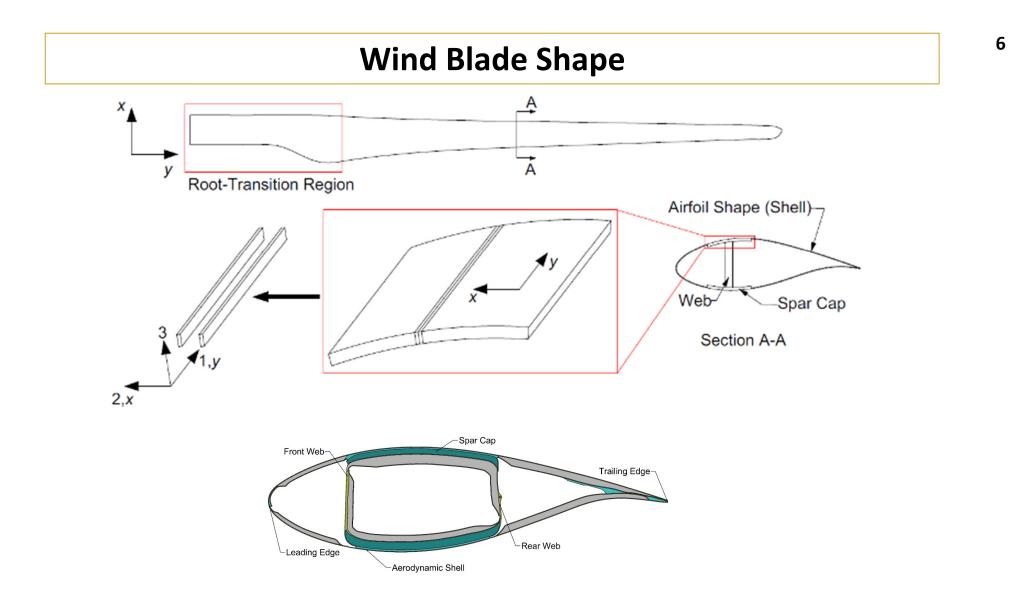


*Bank, Lawrence C., Franco R. Arias, Ardavan Yazdanbakhsh, T. Russell Gentry, Tristan Al-Haddad, Jian-Fei Chen, and Ruth Morrow (2018). "Concepts for reusing composite materials from decommissioned wind turbine blades in affordable housing." *Recycling* 3, no. 1.

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□ Can a decommissioned wind blade be used as a POWER POLE?



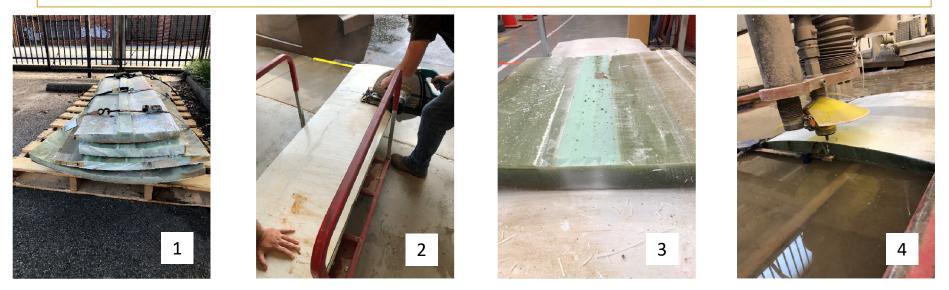


□ 1.5 MW GE 37 Wind Turbine Blade

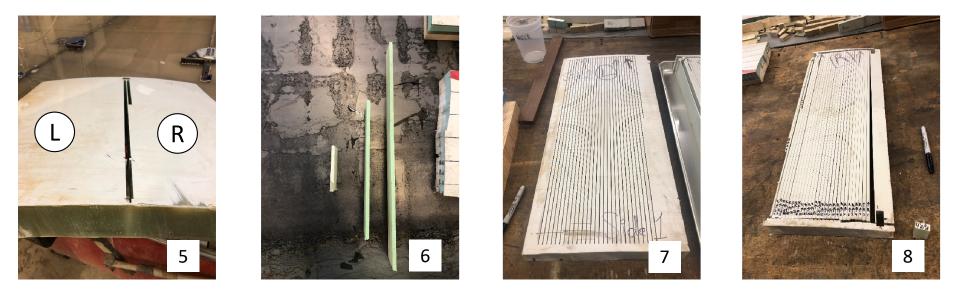




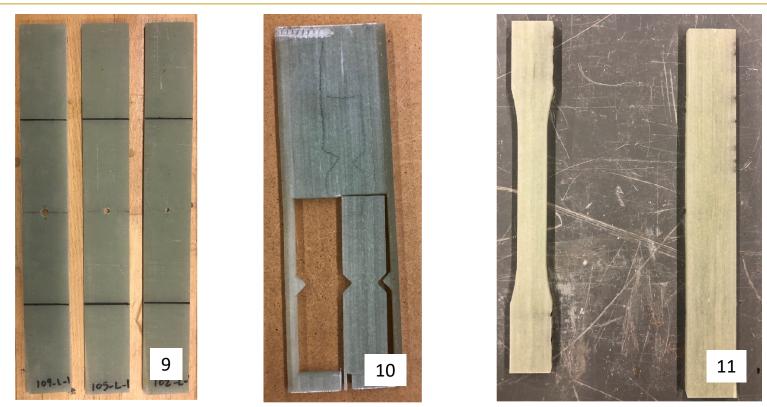
7



- 1. As-received spar cap materials from Logisticus.
- 2. Initial cross-cutting of spar cap slabs.
- 3. Assessment of specimen flatness and removing central bonding material.
- 4. Fixturing of materials on waterjet cutter.

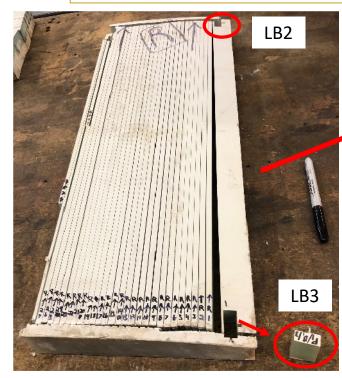


- 5. First cut to reduce width of spar cap and flatten specimen.
- 6. Initial coupons removed from specimen.
- 7. and 8. Specimen fully cut into sections.



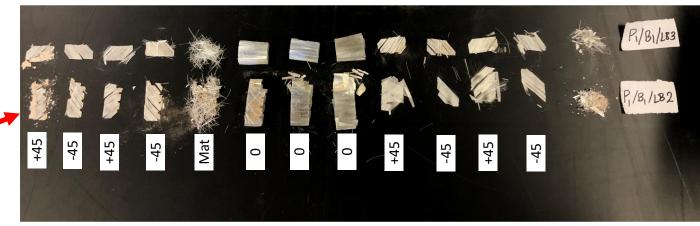
- 9. Fabrication of Open-Hole Tensile specimen
- 10. Fabrication for V-Notch Shear testing
- 11. Fabrication of Dogbone and Straight-Sided Tensile specimens

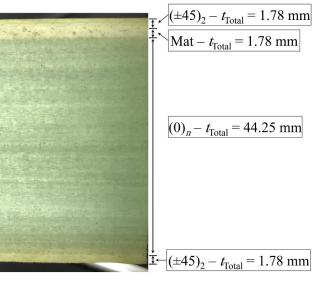
Laminate Characterization Testing



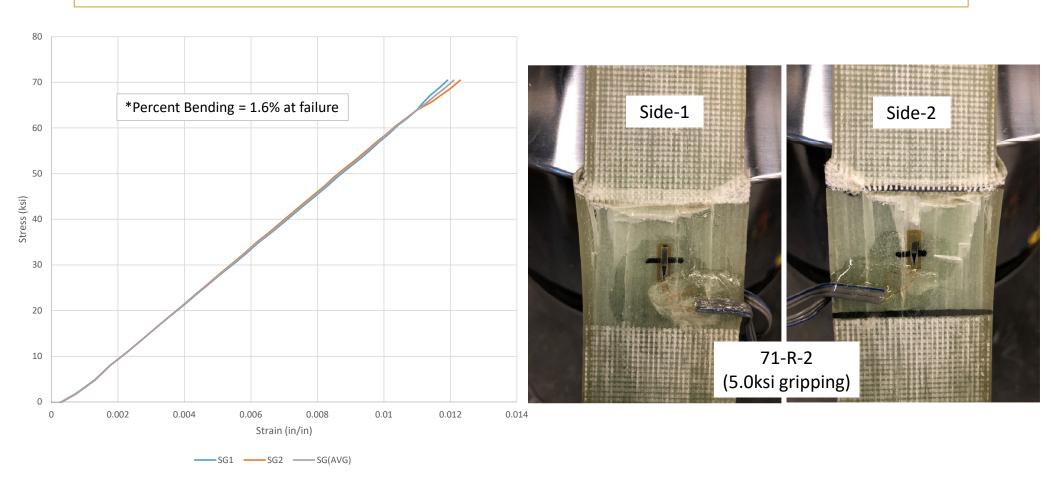
*ASTM 2584 - Standard Test Method for Ignition Loss of Cured Reinforced Resins

*ASTM 3171 - Standard Test Methods for Constituent Content of Composite Materials



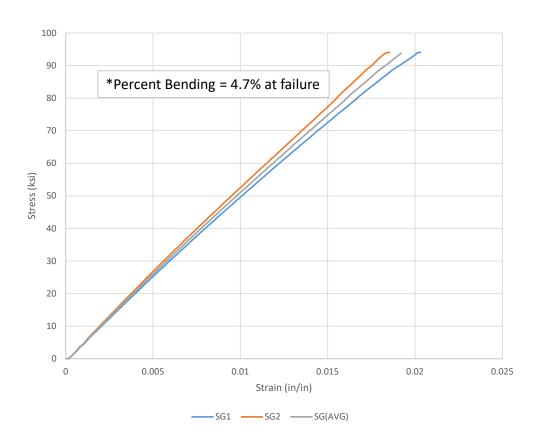


Compressive Testing



*Testing per ASTM D3410 - Standard Test Method for Compressive Properties of Polymer Matrix Composite Materials with Unsupported Gage Section by Shear Loading

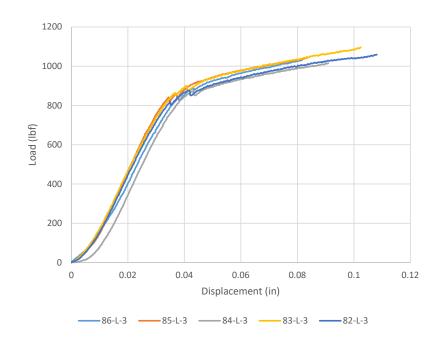
Tensile Testing



*Testing per ASTM D3039 - Standard Test Method for Tensile Properties of Polymer Matrix Composite Materials

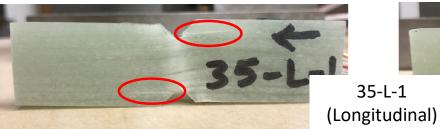


Shear Testing



*Testing per ASTM D5379 - Standard Test Method for Shear Properties of Composite Materials by the V-Notched Beam Method



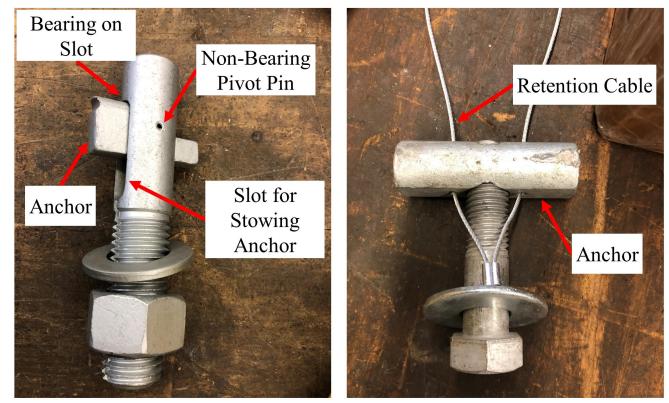




Bolt Testing

- Two blind bolt types; the BlindBolt (24 mm) and the RS BlindNut (19.1 mm).
- For pin-bearing tests; longitudinal (L) and transverse (T) specimens were tested.
- Two spar cap thickness ranges were used;
 - <u>Thin</u> material *ranging from 25.4-35.6 mm* which is the material of the spar cap between 29-32 m from the root of GE37
 - <u>Thick</u> material *ranging from 40.6-55.9 mm* which is the material of the spar cap in the root-transition region of GE37.

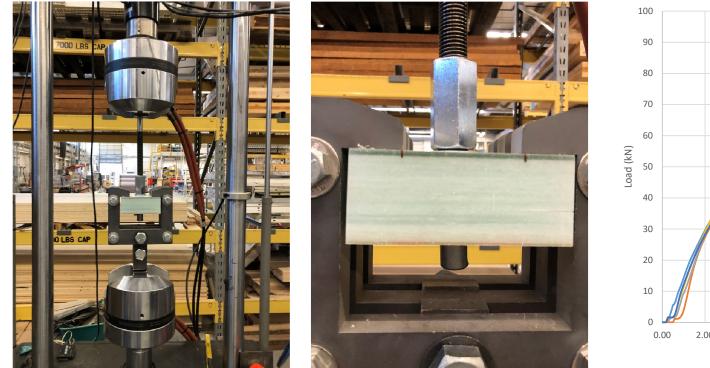
Blind Bolts Types

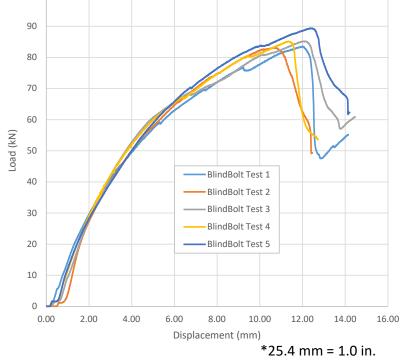


BlindBolt

RS BlindNut

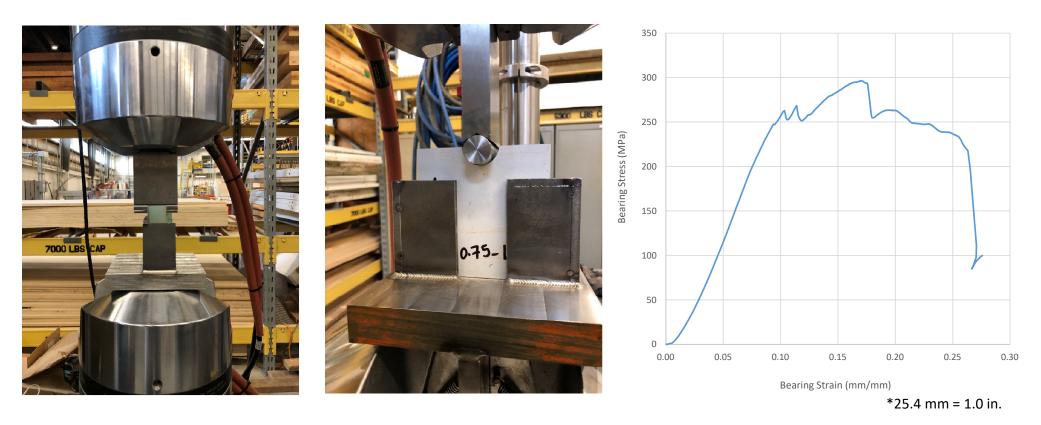
Pull-Out Tests





*Testing per ASTM D7332-Standard Test Method for Measuring the Fastener Pull-Through Resistance of a Fiber-Reinforced Polymer Matrix Composite

Pin-Bearing Tests



*Testing per ASTM D953-Standard Test Method for Pin-Bearing Strength of Plastics

As-Received Strength and Stiffness Compared to Data in the Literature for 100 kW Wind Blades

| Property | Spar Cap of GE37 (V _f = 48-50%) | Sayer et al. (2013) (V _f = unknown) ^(a) | Ahmed et al. (2021) (V _f = 38-43%) ^(b) |
|---|---|--|---|
| Longitudinal Tensile Strength (MPa) | 597 | 477 | 350 |
| Longitudinal Compressive Strength (MPa) | 504 | 447 | 225 |
| Interlaminar Shear Strength (MPa) | 55.0 | 32.3 | - |
| Longitudinal Tensile Modulus (GPa) | 36.8 | 26.7 | 15.6 |
| Longitudinal Compressive Modulus (GPa) | 42.7 | 26.2 | - |

^(a) After Sayer, F., F. Bürkner, B. Buchholz, M. Strobel, A. M. van Wingerde, H-G. Busmann, and H. Seifert. "Influence of a wind turbine service life on the mechanical properties of the material and the blade." *Wind Energy* 16, no. 2 (2013): 163-174.

^(b) After Ahmed, M. MZ, B. Alzahrani, N. Jouini, M. M. Hessien, and S. Ataya. "The Role of Orientation and Temperature on the Mechanical Properties of a 20 Years Old Wind Turbine Blade GFR Composite." *Polymers* 13, no. 7 (2021): 1144.

Conclusions

- This work presents results of tests of the GFRP material spar cap of a 1.5 MW decommissioned GE37 wind turbine blade for tensile, compressive, shear, bearing, and pull-through properties.
- Strength and stiffness properties of the GE37 after 11 years in a wind farm provide values which <u>outperform</u> the data published previously on 100 kW fatigued wind blades. More testing with age and capacity is still needed to judge strength and stiffness retention levels.
- Future work will focus on:
 - EXPERIMENTAL TESTING of other parts (shell, web) and other critical material properties (tension, shear, bending, ...).
 - LARGE-SCALE PHYSICAL tests for potential reuse application(s).

Future Work



Prototype at DFL

Planned Four-Pole Configuration in a wind farm in Kansas